



PROJECT BASED LEARNING SYNOPSIS

On

“Converting ICE four-wheeler to electric vehicle”

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Chapter 1: Details of the Team members

S.No	Name	Engineering Field	Occupation	Role in Project
1.	S SARAVANAN	Electrical and Electronics	Student	Calculations, Checking correctness, information gathering and Preparing synopsis
2.	SUSHANT MAYEKAR	Mechanical	Evaluator	Preparing synopsis and information gathering
3.	RAHUL RAJIV RANJAN	B.Computer science	Student	Preparing synopsis and information gathering
4.	NITIN VITTHALRAO RANE	Mechanical	Student	Thermal Calculation
5.	SHUBHAM KISAN SARPATE	Mechanical	Student	Thermal Calculation

Chapter 2: Project Description



Fig: 1

The objective of the project is to create a step-by-step process that can be repeated and used by others too converting an ICE vehicle to an Electric Vehicle by replacing its IC engine and fuel system with an electric motor coupled with a traction battery. It would be an effective way of reusing the IC engine vehicles then going to scrap for reprocessing and it also eco-friendly. The vehicle selected for project is Maruti Swift because it has low maintenance cost and decent interiors.

The conversion requires removing the engine from the car and all other associated hardware such as fuel tank, exhaust, starter, transmission system (excluding the final drive), clutch and the radiator.

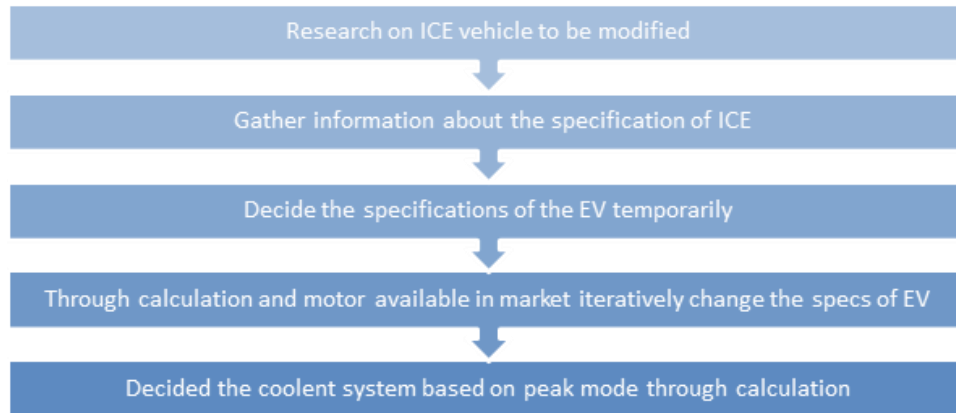
As well as inclusion of traction motor, traction battery pack, BMS, charge port (On-board charger, External charger), power electronics controller, and vehicle control unit is needed.

Expected Krebs weight of the vehicle will be 1100kg (by removing the engine, cultch, transmission system (excluding final drive), fuel tank and engine

control system).

Battery Chemistry is Li-ion (Panasonic cylinder cell) with capacity of 70Ah and voltage of 416V. The vehicle will have range of 170-210km (verified by MIDC) with top speed of 110km/h and acceleration time (0-100km/h) of 12.6 sec*.

Chapter 3: Research Methodology



This project began by surveying and researching available ICE cars in order to find the optimal ICE vehicle for the project.

Once a decision was made, the requirements needed for conversion were acquired.

Then, in order to get the EV up and running, assumptions were made about its specs. evaluated the forces operating on the vehicle to determine the traction force and torque needed for vehicle traction.

Motors available in market were researched, and EV parameters were altered based on calculations and available motors.

Battery capacity decided based on motor needs, range, and available space.

Finally, the calculation data is used to design the isolation and cooling systems.

Chapter 4: Calculation

Maruti Suzuki Swift (2021):

Power= 83BHP @6000 RPM
=61893.1W

Torque= 115 @4000 RPM

Mileage (on avg) =18km/L

Tires-185/65 R15

Top speed=165km/h

Acceleration time (0-100km/h) = 12.6 sec

Transmission type-Manual/automatic

Gear ratio (final drive) - 4.388

Kerb weight= 875-905 kg

Length

3845 mm

Width

1735 mm

Height (Unladed)

1530 mm

Front area = $0.85 \times 1.735 \times 1.53$
=2.26 m²

Cd= 0.34

ICE---> Electric specification:

Battery voltage =416V

Chemistry- Li-Ion

Kerb weight= 1100kg (by removing the engine, cultch and transmission system (excluding final drive), fuel tank and engine control system)

Top speed =110km/h

Range=175-210km (Verified using MIDC)

Acceleration time (0-100km/h) =12.6 sec

Calculation:

Tire radius= $15 \text{ in} / 2 + 18.5 \times .65$

$$=0.31m$$

$$\text{Mass factor} = 1 + 0.04 + 0.0025Ntf^2 \\ = 1.0881$$

$$\text{Total mass} = (\text{kerb mass} * \text{mass factor}) + \text{driver avg weight} \\ = 1100 * 1.0881 + 75 \\ = 1275kg$$

$$F_{\text{tract}} = F_a + F_{rr} + F_D + F_g$$

$$F_g = 0 \text{ (considering travelling in flat surface)}$$

$$F_a = m * a \\ = 1275 * 100 / (3.6 * 12.6) \\ = 2810.85N$$

$$F_{rr} = \mu * m * g \\ = 0.01 * 1275 * 9.81 \\ = 125.08N$$

$$F_D = 0.5 * \rho * C_D * A * V^2 \\ = 0.5 * 1.2 * 0.36 * 2.42 * (110/3.6)^2 \\ = 430.4463N$$

$$F_{\text{tract}} = 3366.38N$$

While considering the gradient force F_g

$$\theta_{\text{max}} = 15 \text{ degree}$$

$$F_g = m * g * \sin(\theta) \\ = 1275 * 9.81 * \sin(15) \\ = 3235.64N$$

As the car climb the uphill the velocity will be less on avg would be 30Km/h

$$\text{So } F_{\text{tract}} = F_a + F_{rr} + F_D + F_g \quad (\text{while climbing up hill acceleration would be less round 0.3 to 0.5}) \\ = 635.955 + 125.08 + 32.02 + 2915.458 \quad (\text{Vehicle max Gradeability restricted to 9.8 based on excel calculation})$$

$$= 2915.458N$$

While consider the max gradient at 30 km/h and $0.5m^2/s$ acceleration we get the as $F_{\text{tract}} = 3708.914$, Power required = 31KW, and Torque required = 1149Nm (but this case is every rare as max inclination in roads is 3 degrees and our motor can supply the required power and torque)

Vehicle Specifications									
kerb mass (kg)	1100								
g (m/s ²)	9.81								
Roll Res μ	0.01	mass factor	1+0.04+0.0025Ntf ²	1.0881					
Cd (Drag)	0.34								
Dens ρ (kg/m ³)	1.2	Driver and added mass (kg)	315				gradient max (degree)	0	
Top speed(km/h)	90								
Acc(0-100Kmph)(m/s ²)	1								
Tire radius	0.31	Total mass (kg)	1515						
Proj Area A (m ²)	2.26								
Nf	4.388								
Drive cycle	MIDC-4W								
FORCES ACTING									
Fd(nm)	m*a	1515							
Frr(nm)	$\mu*m*g$	148.6215							
Fg(nm)	$0.5*\rho*C_d*A*V^2$	288.15							
Fa(nm)	$m*g*\sin(\Theta)$	0							
Ft(nm)	Fd+Frr+Fa+Fg	1951.772							
Power and Torque required									
Peak Power (KW)	Force*velocity	49							
Peak Torque (Nm)	Force*Tire radius	605.0492							

Fig: 2

Energy Consumption:

As per MIDC cycle the max speed is 90 km/h and for approx 20 min (1180 sec). As the vehicle limited with top speed as 110km/h, so the max speed in MIDC is consider to be 80km/h (advisable speed of the converted electric vehicle).

$E_{avg}=94\text{Wh/Km}$ (without regenerative breaking)

$E_{avg}=86.63\text{ Wh/km}$ (considering regenerative breaking of 30%)

$E_{total}= E_{avg} + E_{aux}$

$=86.63+30$

$\sim 117\text{ Wh/Km.}$

While consider all the factors

- 1) Passenger and luggage weight (75*4 kg+15kg)
- 2) Inefficiency
- 3) Considering DOD as 80%

Cell Voltage= 3.6 V

Cell Capacity= 3.2 Ah

Internal Resistance= 45mΩ

Charging and discharging rate=1C

DOD =85%

V_{pc} =volume of cell

$V_{pc}=\pi*(d/2)^2 * L$

$=\pi*(0.0185/2)^2 *0.0653$

$=17.55\text{cm}^3$

$E_{\text{cell}}=V *Ah$

$=3.6*3.2$

$=11.52\text{Wh}$

$E_b=E_{\text{avg}} * \text{Range}$

$=117*200$ (Consider only with driver mass and without considering the inefficiency)

$=23.4\text{KWh}$

E_b (considering DOD% of 80) = $23.4/.8$ (considering for worst for case scenario)

$=29.25\text{KWh}$

No. of cell in series = $416\text{V}/3.6$

~ 116 cells (for cell balancing)

No. of cell in parallel= $23.4\text{Kw}/416*3.2$

$=18$ cells

No. of cell in parallel (considering 1.25 factor for DOD compensation) =

$18*1.25$ or $16/0.8$

$=22$ cells

No. of cells= $116*22$

$=2552$ cells

$E_{\text{cf}}= 23.4*1.25$

$=29.25\text{KWh}$

Battery configuration is 22P116S

Mass of Battery pack=124kg

Battery voltage= 417.6V

Battery capacity=70Ah

Volume of battery pack= 44787.6cm^3 (without cell holder)

Volume of battery pack adding cell holder will be $=2*2*7*2552$
 $=71456\text{cm}^3$

Battery dimension will be

$L = \text{cell holder length} * 128$

$= 2 * 116$

$= 232\text{ cm}$

$W = \text{cell holder width} * 22$

$= 2 * 20$

$= 44\text{cm}$

$H = 6.53\text{cm}$

Hood space dimension is $600\text{mm} * 400\text{mm} * 350\text{mm}$ ($L * W * H$).



Fig: 4

Volume of the hood after removing the engine, transmission, battery, radiator etc. is,

Volume of the hood is 84000cm^3 .

As the Length and Width of battery pack exceed the length and Width of the hood,

Let's divide the battery pack into 4 modules of configuration 22P29S

So dimension of modules will be

$L = 29 * 2$

$= 58\text{cm}$

$W = 22 * 2$

$= 44\text{cm}$

$H = 8$ (considering bus bar, plastic mold, base plate, wire harness)

Now we need to connect the modules in series in order to achieve 22P116S configuration.

It is done placing modules top over the other.

As the height of the hood is 35cm and 4 module with height will be about 32cm (may be little more) which will fit inside hood.

Motor spec					
Motor rated power (KW)	22			Top speed required (KM/h)	110
Motor peak power (KW)	55			Peak torque required (Nm)	1150
Motor rated voltage (V)	336			final drive G.R of vehicle	4.388
Motor rated current (A)	65.47619048			G.R of reducer	2.24
Motor peak current (A)	163.6904762			Gear efficiency of F.D	0.94
Motor rated Torque (NM)	60			Gear efficiency of reducer	0.9
Motor peak Torque (NM)	140			Tire radius (m)	0.31
Motor rated speed (rpm)	4050				
Motor peak speed (rpm)	11000				
				obtained torque (peak) Nm	1164.160973
				obtained speed (peak) km/h	110.6392528
Cell spec					
Cell length (m)	0.0653				
Cell diameter (m)	0.0185			Cell volume ($\pi \cdot (d/2)^2 \cdot L$) in Cm ³	17.55280465
Cell Mass (kg)	0.0485			Cell energy Wh	11.52
Cell Voltage (V)	3.6				
Cell Capacity (Ah)	3.2			Energy required (KWH)	23.4
				TOTAL Energy required (dod compensation and losses)	29.25
Charging and discharging rate	1C				
dod	0.8			Battery volume (cm	71456
				battery mass (kg)	123.772
no of cell in series	94				
no of cell in parallel	21				
No of cells	1974				
lets round of no of cell to get desired number so that the battery pack can fit inside the hood					
				Available volume inside the hood cm ³	84000
no of cell in series	116				
no of cell in parallel	22				
no. of cells	2552				
battery volume without cell holder/insulator cm ³	44794.75746				
battery volume with cell holder/insulator cm ³	71456				

Fig: 5

Power required in motor (P_m) = $F_{\text{tract}} \cdot V$

Let take $V_{\text{max}} = 110 \text{ Km/h}$

$P_{m(\text{max})} = 3366.38 \cdot 110/3.6$

=145KW (But this will not be the case)

In above case @ 110Km/h which is the top speed, acceleration factor is considered. Which means speed will increase above the top speed which is not possible, so considering this the peak power was untainted with the help of Microsoft excel.

Vehicle Specifications								
kerb mass (kg)	1100							
g (m/s ²)	9.81							
Roll Res μ	0.01	mass factor	1+0.04+0.0025Ntf ²	1.0881				
Cd (Drag)	0.34							
Dens ρ (kg/m ³)	1.2	Driver and added mass (kg)	315			gradient max (degree)		0
Top speed(km/h)	90							
Acc(0-100Kmph)(m/s ²)	1							
Tire radius	0.31	Total mass (kg)	1515					
Proj Area A (m ²)	2.26							
Nf	4.388							
Drive cycle	MIDC-4W							
FORCES ACTING								
Fd(nm)	m*a	1515						
Frr(nm)	$\mu*m*g$	148.6215						
Fg(nm)	$0.5*\rho*C_D*A*V^2$	288.15						
Fa(nm)	$m*g*\sin(\Theta)$	0						
Ft(nm)	Fd+Frr+Fa+Fg	1951.772						
Power and Torque required								
Peak Power (KW)	Force*velocity	49						
Peak Torque (Nm)	Force*Tire radius	605.0492						

Fig: 6

Vehicle Specifications								
kerb mass (kg)	1100							
g (m/s ²)	9.81							
Roll Res μ	0.01	mass factor	1+0.04+0.0025Ntf ²	1.0881				
Cd (Drag)	0.34							
Dens ρ (kg/m ³)	1.2	Driver and added mass (kg)	400			gradient max (degree)		0
Top speed(km/h)	10							
Acc(0-100Kmph)(m/s ²)	2.21							
Tire radius	0.31	Total mass (kg)	1596.91					
Proj Area A (m ²)	2.26							
Nf	4.388							
Drive cycle	MIDC-4W							
FORCES ACTING								
Fd(nm)	m*a	3529.171						
Frr(nm)	$\mu*m*g$	156.6569						
Fg(nm)	$0.5*\rho*C_D*A*V^2$	3.557407						
Fa(nm)	$m*g*\sin(\Theta)$	0						
Ft(nm)	Fd+Frr+Fa+Fg	3689.385						
Power and Torque required								
Peak Power (KW)	Force*velocity	10						
Peak Torque (Nm)	Force*Tire radius	1143.709						

Fig: 7

$$p_{m(max)} = 40-50KW$$

Torque required for motor(T_m) = $F_{tract} * \text{wheel radius} / G.R$ (with the final drive ratio)

$$T_m = 3366 * 0.31 / 4.388$$

$$= 237.82 \text{ Nm}$$

Motor selected:

PMSM motor from - RAWSUNS power generation and propulsion solution.

Model: R55-140

Specification:

Motor rated power (KW)	22
Motor peak power (KW)	55
Motor rated voltage (V)	336
Motor rated current (A)	66
Motor peak current (A)	165
Motor rated Torque (NM)	60
Motor peak Torque (NM)	140
Motor rated speed (rmp)	4050
Motor peak speed (rmp)	11000

Table: 1

Even with a final drive gear ratio, motor torque will not satisfy the required torque, i.e., 1150Nm. So a reducer with a gear ratio of 2.24 is added. (Obtained from calculations and assumptions made with the help of Microsoft Excel).

Thermal Calculation:

Battery configuration is 22P116S.

Battery pack of 4 with a configuration of 22P29S (connected in series).

Cell internal resistance (I_r) is 45m Ω .

Cell capacity=3.2Ah

$$\begin{aligned}
 \text{Heat generated by a cell } (Q_{\text{cell}}) &= I^2 * I_r \\
 &= 3.2^2 * 45 * 10^{-3} \\
 &= 0.4608 \text{ W}
 \end{aligned}$$

Pack configuration 22P29S

$$\begin{aligned}
 \text{Heat generated in pack } (Q_{\text{pack}}) &= I^2 * I_r * \text{no. of cells in pack} \\
 &= 3.2^2 * 22 * 29 * 45 * 10^{-3} \\
 &= 294 \text{ W}
 \end{aligned}$$

$$\begin{aligned}
 \text{Heat generated by battery } (Q_B) &= 4 * 294 \\
 &= 1176 \text{ W}
 \end{aligned}$$

Peak heat generated by Battery would be 165A so each cell discharge at nearly

2.23C, so let take discharge rate as 2.5C to round it up

$$Q_{(\text{peak B})} = (2.5 \times 3.2)^2 \times 4 \times 22 \times 29 \times 45 \times 10^{-3}$$

$$= 7349.76 \text{ W}$$

Battery pack dimension is $58 \times 44 \times 8 \text{ cm}$

Area of heat convection area = 4 of $(58 \times 8) + 58 \times 44 \Rightarrow 4408 \text{ cm}^2$ (4 pack of dimension $58 \times 44 \times 8$)

Assuming: The pack temperature is $= 45 \text{ c}$

The ambient temperature is $= 35 \text{ c}$

Thermal resistance, $R_{th} = \Delta T / Q$

$$= T_{\text{Cell}} - T_{\text{ambient}} / 7349.76$$

$$= 45 - 35 / 7349.76$$

$$= 1.3606 \times 10^{-3} \text{ k/w}$$

Convective $R_{th} = 1/h$

$$1.3606 \times 10^{-3} = 1/h \times 4408$$

$$h = 1.6674 \times 10^{-1} \text{ w/cm}^2\text{k (heat transfer coefficient)}$$

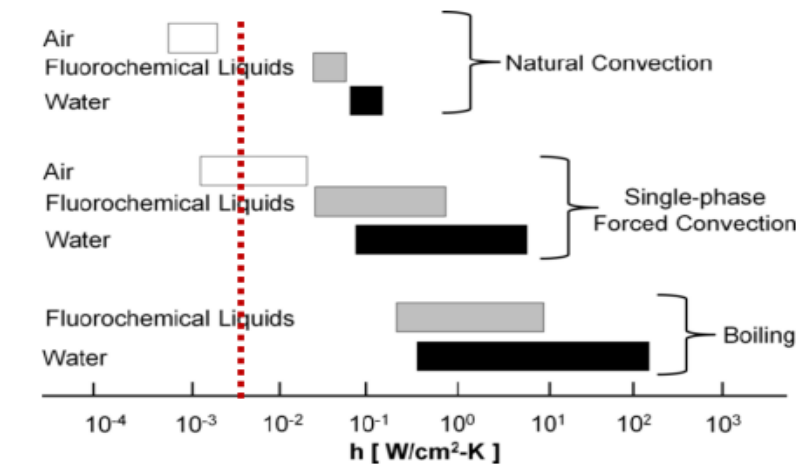


Fig: 8

As the heat transfer coefficient is $1.67 \times 10^{-1} \text{ w/cm}^2 \text{ k}$ forced water convection is preferred.

Chapter 5: Tools Required

1. Microsoft Excel
2. Matlab
3. Maruti Suzuki Showroom manual
4. Internet

References:

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